

# Image Cover Sheet

**CLASSIFICATION**

UNCLASSIFIED

**SYSTEM NUMBER**

142296



**TITLE**

EVALUATION OF A P\ (VDF-TrFE\ ) COPOLYMER WITH FLEXIBLE ELECTRODES  
MANUFACTURED BY AMP SENSORS LTD

**System Number:**

**Patron Number:**

**Requester:**

**Notes:**

**DSIS Use only:**

**Deliver to:** FF



UNLIMITED DISTRIBUTION



**National Defence**  
Research and  
Development Branch

**Défense nationale**  
Bureau de recherche  
et développement

**DREA CR/93/482**

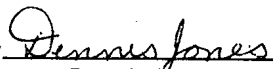
**EVALUATION OF A  
P(VDF-TrFE) COPOLYMER WITH  
FLEXIBLE ELECTRODES  
MANUFACTURED BY AMP SENSORS LTD.**

by

J.E. Haysom - S. Sherrit - H.D. Wiederick - B.K. Mukherjee

**ROYAL MILITARY COLLEGE of CANADA**  
Kingston, Ontario, Canada  
K7K 5L0

Scientific Authority

  
Dennis F. Jones

DREA 098  
Contract Number

January 1994

**CONTRACTOR REPORT**

Prepared for

**Defence  
Research  
Establishment  
Atlantic**



**Centre de  
Recherches pour la  
Défense  
Atlantique**

**Canada**

11/15

### Abstract

The ferroelectric copolymer poly(vinylidene difluoride- trifluoroethylene) shows considerable promise as a transducer material for sonar transducers. This material has a low density, is flexible and has a hydrostatic figure of merit which can be an order of magnitude better than that of lead zirconate titanate which is currently the most commonly used transducer material. We have investigated a 0.500 mm thick copolymer with thin flexible aluminium coated nickel electrodes manufactured by AMP Sensors Ltd of the USA. We have determined the elastic, dielectric, piezoelectric and hydrostatic properties of the copolymer with the flexible electrodes. The hydrostatic voltage coefficient and the hydrostatic figure of merit of this copolymer sample are at least five times better than those of lead zirconate titanate but they are not as good as values for the same copolymer with stiff electrodes which were investigated earlier. These properties have a small dependence on pressure and in this regard the present material is better than other polymers studied earlier. //

### Résumé

Le copolymère de bifluorure de vinylidène avec le trifluoroéthylène est un matériau ferroélectrique qui se révèle prometteur comme matériau pour les transducteurs de sonar. Ce matériau a une faible masse volumique, il est flexible et son facteur de mérite hydrostatique peut être de l'ordre de dix fois mieux que celui du zirconate -titanate de plomb qui est couramment le matériau le plus utilisé dans les transducteurs. Nous avons examiné une feuille, de 0,500 mm d'épaisseur, d'un copolymère, muni des électrodes minces et flexibles du nickel plaqué de l'aluminium, qui est fabriqué par AMP Sensors Ltd des Etats Unis. Nous avons déterminés les constantes élastiques, diélectriques, piézoélectriques et hydrostatiques de l'échantillon de copolymère muni de ces électrodes flexibles. Le coefficient hydrostatique de tension et le facteur de mérite hydrostatique de ce matériau sont au moins cinq fois mieux que ceux du zirconate -titanate de plomb mais ils ne sont pas aussi bons que les coefficients du même copolymère muni des électrodes rigides que nous avons caractérisé avant. Ces propriétés ont une petite dépendance sur la pression hydrostatique mais cette dépendance est plus faible que celle trouvée pour des polymères étudiés auparavant.

UNCLASSIFIED

## 1. INTRODUCTION

Polyvinylidene difluoride (PVDF) is a piezoelectric polymer which offers some advantages over lead zirconate titanate (PZT) as the sensor material of choice for use in sonar transducers. Its advantages include mechanical flexibility, good acoustic impedance matching to water, low cost and ease of construction. The piezoelectric and pyroelectric properties of PVDF are somewhat enhanced if the vinylidene fluoride is copolymerised with trifluoroethylene (TrFE) which appears to make it easier for chains to rotate in the vinylidene fluoride. Sometimes a proper distinction is not made between the copolymer and PVDF and the latter term has been used to describe both materials.

A proprietary commercial copolymer material is manufactured by AMP Sensors Ltd. of Valley Forge, Pennsylvania, USA. The material is initially made in layers of 0.500 mm thickness and up to 5" x 7" (0.127 m x 0.178 m) in area. However thicker tiles can be obtained by laminating the material with or without interleaving electrodes corresponding to their P and S series of product classification respectively. A six inch square sheet of the 0.500 mm copolymer with a flexible electrode of aluminum over nickel was supplied to us by Mr. Mitch Thompson of AMP Sensors Ltd. and this report presents our characterisation of this sample.

It should be noted that, since the copolymer material has a low density and is soft, the effect of the electrodes on its mechanical properties is significant. We have also received samples of copolymer with stiff electrodes from the same company and our characterisation of this material is the subject of a separate report<sup>1</sup>.

## 2. MEASUREMENTS

### 2.1 Specimens

The copolymer sample supplied to us was in the form of a six inch (15.2 cm) square sheet of 0.5 mm thickness with thin flexible electrodes of aluminium coated nickel. From this sheet, five one inch squares were cut and these were used for characterising the material.

### 2.2 Material Constants from Resonance Measurements

Impedance spectra of the samples were analysed using Smits' method<sup>2</sup> which has been outlined in an earlier report<sup>3</sup>. We have analysed the thickness extensional resonances of the specimens to determine the real and imaginary components of the mechanical stiffness at constant dielectric displacement  $c_{33}^D$ , the dielectric constant at constant strain  $\epsilon_{33}^S$ , the piezoelectric coefficient in the poling direction  $h_{33}$ , and the thickness mode electromechanical coupling factor  $k_t$ . In Table 1 we give the averages of our results on the five specimens. Variations between the samples were between 3% and 10% with the exception of the imaginary part of the dielectric constant  $\epsilon_{33}^S$ , which had a variation of up to 28%. In Figure 1 we show the sample impedance scans along with the theoretical fits obtained by using the material constants calculated

UNCLASSIFIED

UNCLASSIFIED

for the specimen.

**Table 1: Average thickness-extensional material constants**

Property	Value
$c_{33}^D$ ( $10^9$ N/m <sup>2</sup> )	6.46(1+0.032i)
$\epsilon_{33}^S$ ( $10^{-11}$ F/m)	3.68(1+0.158i)
$h_{33}$ ( $10^9$ V/m)	3.25(1+0.130i)
$k_r$	0.244(1+0.193i)

In comparison with the values found for the copolymer tiles with stiff electrodes<sup>1</sup>, the values of  $c_{33}^D$  and  $h_{33}$  for this flexible copolymer are higher by factors of about 4 and 2 respectively, the value of the imaginary part of  $k_r$  is almost 4 times larger whereas that of  $\epsilon_{33}^S$  is somewhat smaller. These differences are caused by the fact that the stiff electrodes are thicker and increase the mass of the electrode-polymer composite; this effect is consistent with earlier observations in the case of PVDF samples obtained from the RAYTHEON company<sup>4</sup>.

An attempt was made to study the thickness length resonance in the copolymer and to study the effects of varying the aspect ratio (defined as the length divided by the width) of the specimens. Tiles of the copolymer were cut in 6.0 cm lengths, with aspect ratios of 10 and 20. These tiles were cut with their lengths both parallel and perpendicular to a chosen edge of the supplied sheet in order to check possible anisotropy in the 1 and 2 directions which might have been caused by stretching or other processes during production of the material. The presence of anisotropy would cause different levels of resonance peaks in the samples cut in different directions. However, the length resonance peaks could not be detected in the impedance scans and hence no conclusions could be drawn about the material constants governing these resonances. The absence of the resonance peaks is likely to be due to the clamping effects of the electrodes on the soft copolymer samples.

### 2.3 The Low Frequency Dielectric Constant

The low frequency capacitances of the samples were measured at a frequency of 400 Hz with the help of a Hewlett Packard 4192A Impedance Analyser and the results were used to find the average low frequency permittivity and the average dielectric constant of the material:

$$\epsilon_{33}^T = 6.71 \times 10^{-11} \pm 1\% \text{ F/m} \quad \text{and} \quad \frac{\epsilon_{33}^T}{\epsilon_0} = 7.58 \pm 1\% .$$

The low frequency dissipation was found to be less than 2%. Our results on the permittivity and the dissipation agree well with our earlier measurements on the AMP copolymer tiles with the stiff

UNCLASSIFIED

UNCLASSIFIED

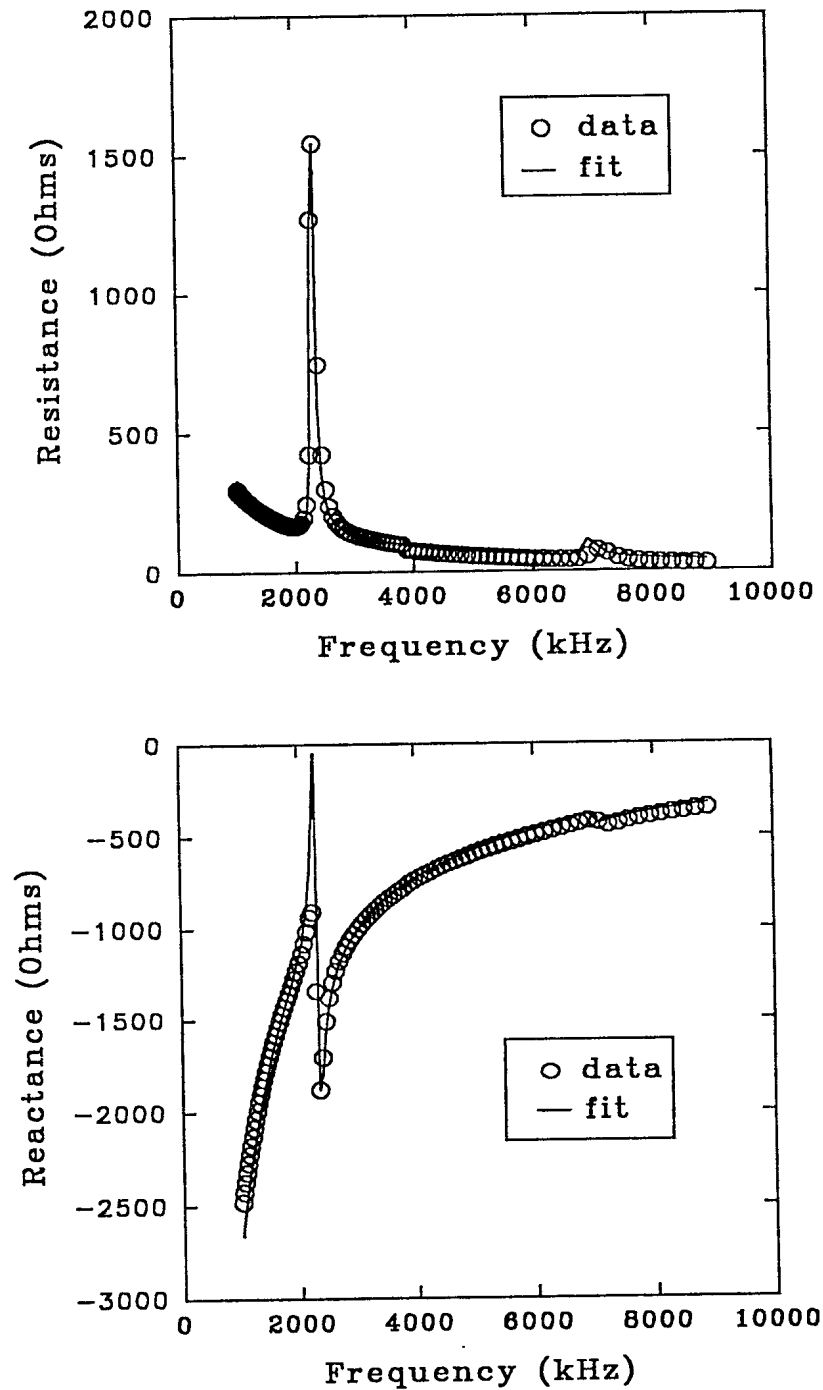


Figure 1. The real and imaginary parts of a typical frequency spectrum of the thickness-extensional resonance of a poled copolymer sample. The measurements were carried out at 22°C. The points represent measurements and the line is the fit obtained by using the material constants determined from the measurements.

UNCLASSIFIED

## UNCLASSIFIED

electrodes<sup>1</sup> and with measurements by Wang et al on similar clamped copolymer tiles<sup>5</sup>.

#### **2.4 Measurement of the Piezoelectric Charge Constant in the 33 Direction**

The value of  $d_{33}$  was obtained using a 1 cm<sup>2</sup> force head on a Berlincourt type meter which was operated at a frequency of 200 Hz. Table 2 shows values of  $d_{33}$  for our five samples of copolymer. These results yield an overall average value of  $29 \pm 12\%$  pC/N which may be compared with the value of 24.75 pC/N found by Wang et al<sup>5</sup>.

**Table 2: Measured values of  $d_{33}$  for the five samples**

sample	1	2	3	4	5
$d_{33}$ (pC/N)	27.2	30.6	31.0	29.4	26.7

#### **2.5 Hydrostatic Measurements**

The hydrostatic voltage coefficient,  $g_h$ , was measured as a function of pressure at a temperature of 20° C using a frequency of 400 Hz. The hydrostatic figure of merit which is the product of the hydrostatic voltage and charge coefficients is given by  $g_h d_h = g_h^2 \epsilon_{33}^T$ . Table 3 gives the average values of both the hydrostatic voltage coefficient and the hydrostatic figure of merit for pressures between 2 MPa and 14 MPa while figures 2 and 3 show the variation of these quantities as a function of pressure.

**Table 3: Average hydrostatic coefficients**

pressure (MPa)	$g_h$ ( $10^{-3}$ Vm/N)	$g_h d_h$ ( $10^{-15}$ Pa <sup>-1</sup> )
2	140 ± 3%	1310 ± 6%
4	134 ± 3%	1200 ± 6%
6	132 ± 3%	1170 ± 6%
8	130 ± 2%	1130 ± 4%
10	129 ± 2%	1110 ± 4%
12	128 ± 2%	1100 ± 4%
14	127 ± 2%	1080 ± 4%

We note that both the hydrostatic voltage coefficient and the figure of merit decrease as a function of pressure. As between pressures of 2 MPa and 14 MPa, the hydrostatic voltage coefficient decreases by

UNCLASSIFIED



UNCLASSIFIED

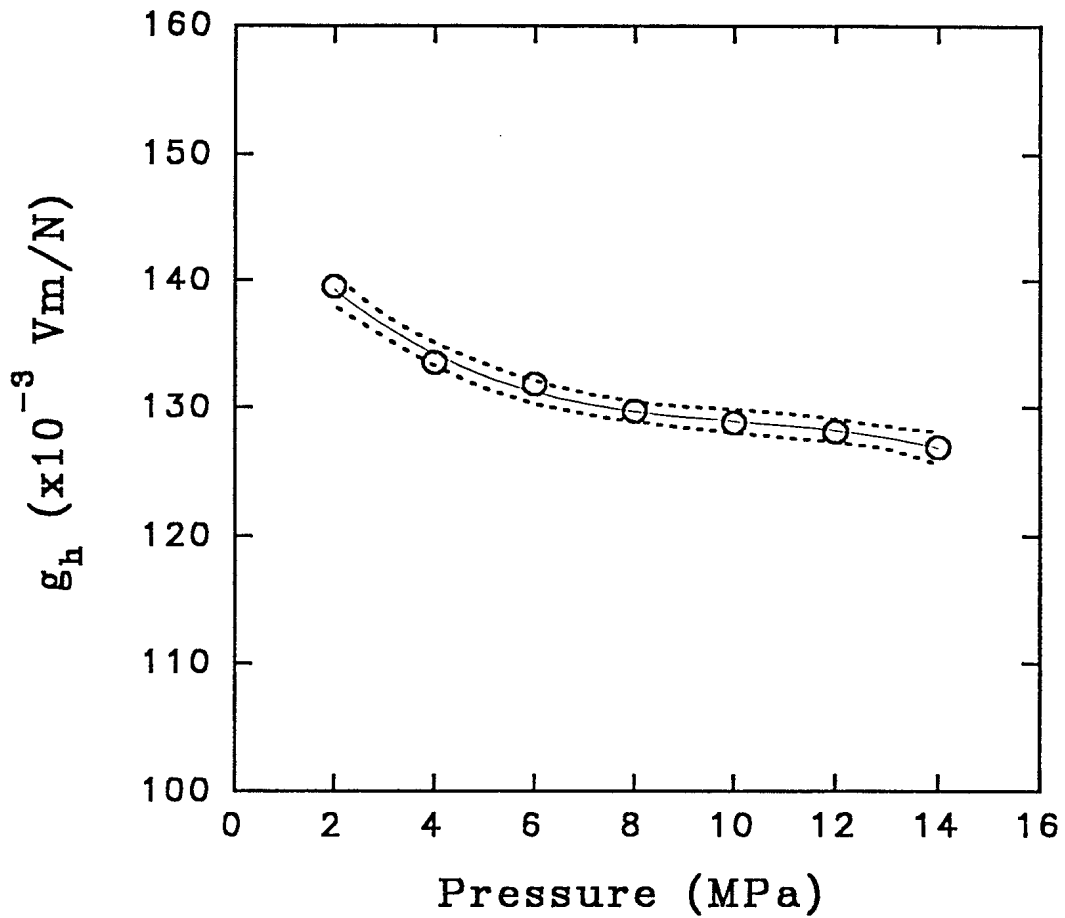


Figure 2. The pressure dependence of the average hydrostatic voltage coefficient,  $g_h$ , of the copolymer showing data and the polynomial fit to the data with the 95% confidence limits shown as dotted lines.

UNCLASSIFIED

UNCLASSIFIED

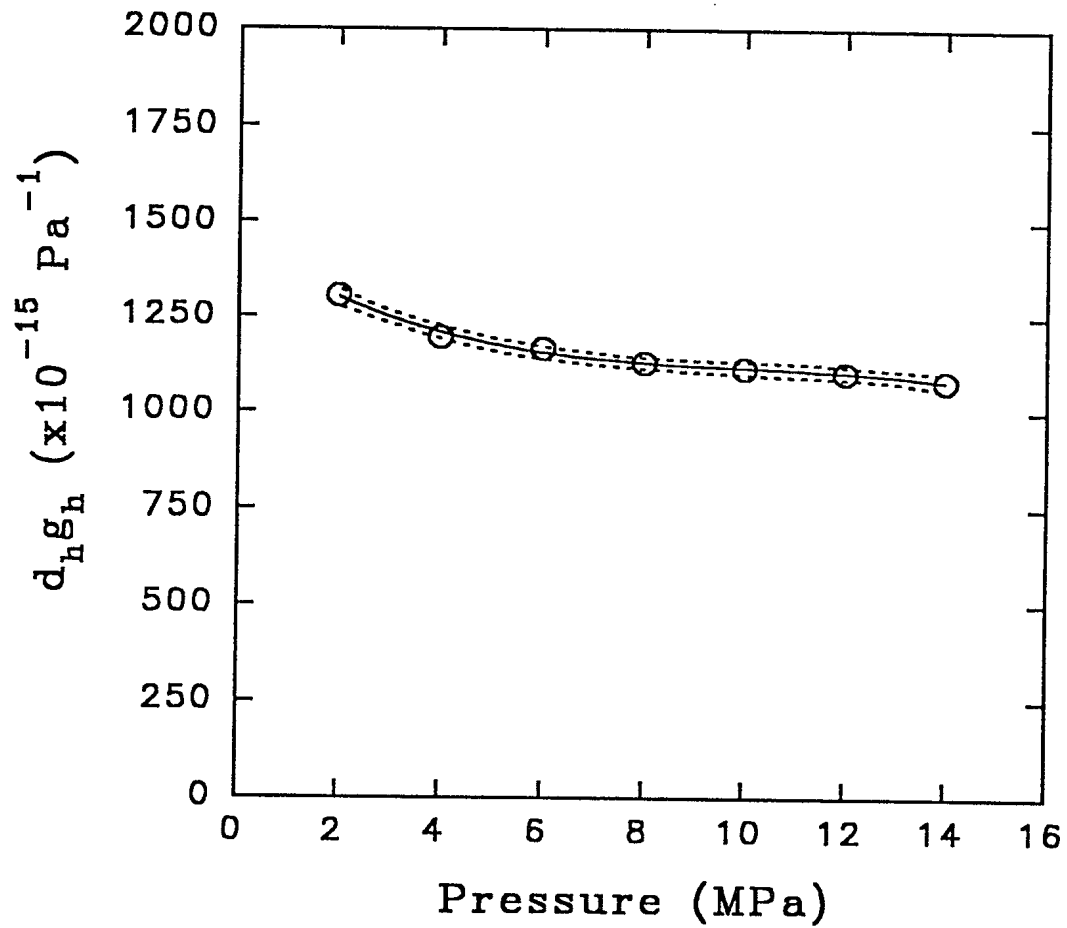


Figure 3. The pressure dependence of the average figure of merit,  $g_h d_h$ , of the copolymer showing data and the polynomial fit to the data with the 95% confidence limits shown as dotted lines.

UNCLASSIFIED

UNCLASSIFIED

around 9% and the figure of merit decreases by about 17% and these values are not very different from the values which we obtained for the copolymer with thick electrodes<sup>1</sup>. The variation could be fit by polynomials as follows:

$$g_h = a_3 P^3 + a_2 P^2 + a_1 P + a_0$$

with

$$a_0 = 147.24 (10^{-3} \text{ Vm/N}), a_1 = -4.808 (10^{-3} \text{ Vm/(N(MPa))})$$

$$a_2 = 0.4435 (10^{-3} \text{ Vm/(N(MPa)}^2\text{)}), a_3 = -0.0114583 (10^{-3} \text{ Vm/(N(MPa)}^3\text{)})$$

and

$$d_h g_h = b_3 P^3 + b_2 P^2 + b_1 P + b_0$$

with

$$b_0 = 1447.7(10^{-15} \text{ Pa}^{-1}), b_1 = -88.440(10^{-15} \text{ Pa}^{-1})/(\text{MPa})$$

$$b_2 = 8.2274(10^{-15} \text{ Pa}^{-1})/(\text{MPa}^2), b_3 = -0.27083,(10^{-15} \text{ Pa}^{-1})/(\text{MPa}^3)$$

where  $P$  is the pressure in MPa,  $g_h$  is in  $10^{-3} \text{ Vm/N}$  and  $g_h d_h$  is in  $10^{-15} \text{ Pa}^{-1}$ . The fits of these polynomials to the data are shown in figures 2 and 3 which also show the 95% confidence curves for the polynomials.

### 3. CONCLUSIONS

We have characterised the dielectric, piezoelectric and hydrostatic properties of 0.500 mm thick P(VDF-TrFE) copolymer with flexible electrodes manufactured by AMP Sensors Ltd. The hydrostatic coefficients are at least a factor of 5 better than those of lead zirconate titanate (PZT). However these coefficients show a small decrease as a function of pressure and they are not as good as the hydrostatic properties of a similar copolymer with stiff electrodes. Purely on the basis of their hydrostatic properties, it would appear that the S series copolymer with thick electrodes, on which we have reported earlier<sup>1</sup>, is the better material for use in sonar transducers.

UNCLASSIFIED

UNCLASSIFIED

#### 4. REFERENCES

1. J.E. Haysom, S. Sherrit, B.K. Mukherjee and H.D. Wiederick, "Evaluation of P(VDF-TrFE) Copolymer Tiles with Stiff Electrodes Manufactured by AMP Sensors Ltd", *Defence Research Establishment Atlantic Contractor Report CR/93/481*, (1993).
2. J.G. Smits, "Iterative Method for the Accurate Determination of the Real and Imaginary Parts of the Material Constants for Piezoelectric Ceramics", *IEEE Trans. on Sonics and Ultrasonics*, SU-23, 393-402 (1976).
3. B.K. Mukherjee, H.D. Wiederick and S. Sherrit, "Establishment of a Laboratory to Characterise Piezoelectric Materials", *Defence Research Establishment Atlantic Contractor Report CR/90/439*, (1990).
4. S. Sherrit, J.E. Lauzon, H.D. Wiederick and B.K. Mukherjee, "Evaluation of a Thick PVDF Sheet Made by RAYTHEON", *Defence Research Establishment Atlantic Contractor Report CR/93/439* (1993).
5. H. Wang, Q.M. Zhang, L.E. Cross and A.O. Sykes, "Piezoelectric, Dielectric and Elastic Properties of Poly(Vinylidene Fluoride/Trifluoroethylene)", *J. Appl. Phys.*, 74, 3394-3398 (1993).

UNCLASSIFIED

**UNCLASSIFIED**  
SECURITY CLASSIFICATION OF FORM  
(highest classification of Title, Abstract, Keywords)

<b>DOCUMENT CONTROL DATA</b>		
(Security classification of title, body of abstract and indexing annotation must be entered when the overall document is classified)		
<b>1. ORIGINATOR</b> (the name and address of the organization preparing the document. Organizations for whom the document was prepared, e.g. Establishment sponsoring a contractor's report, or tasking agency, are entered in section 8.)  <b>Royal Military College of Canada Kingston, Ontario</b>	<b>2. SECURITY CLASSIFICATION</b> (overall security classification of the document including special warning terms if applicable).  <p style="text-align: center; font-size: large;">Unclassified</p>	
<b>3. TITLE</b> (the complete document title as indicated on the title page. Its classification should be indicated by the appropriate abbreviation (S,C,R or U) in parentheses after the title).  <p style="text-align: center; font-size: large;">Evaluation of a P(VDF-TrFE) copolymer with flexible electrodes manufactured by Amp Sensors Ltd.</p>		
<b>4. AUTHORS</b> (Last name, first name, middle initial. If military, show rank, e.g. Doe, Maj. John E.)  <p style="text-align: center; font-size: large;">J.E. Haysom, S. Sherrit, H.D. Wiederick, and B.K. Mukherjee</p>		
<b>5. DATE OF PUBLICATION</b> (month and year of publication of document)  <p style="text-align: center; font-size: large;">January 1994</p>	<b>6a. NO OF PAGES</b> (total containing information include Annexes, Appendices, etc.)  <p style="text-align: center; font-size: large;">9</p>	<b>6b. NO. OF REFS</b> (total cited in document)  <p style="text-align: center; font-size: large;">5</p>
<b>7. DESCRIPTIVE NOTES</b> (the category of the document, e.g. technical report, technical note or memorandum. If appropriate, enter the type of report, e.g. interim, progress, summary, annual or final. Give the inclusive dates when a specific reporting period is covered).  <p style="text-align: center; font-size: large;">Contractor Report</p>		
<b>8. SPONSORING ACTIVITY</b> (the name of the department project office or laboratory sponsoring the research and development. Include the address).  <p style="text-align: center; font-size: large;">Defence Research Establishment Atlantic</p>		
<b>9a. PROJECT OR GRANT NO.</b> (if appropriate, the applicable research and development project or grant number under which the document was written. Please specify whether project or grant).  <p style="text-align: center; font-size: large;">1AU-12</p>	<b>9b. CONTRACT NO.</b> (if appropriate, the applicable number under which the document was written).  <p style="text-align: center; font-size: large;">DREA098</p>	
<b>10a. ORIGINATOR'S DOCUMENT NUMBER</b> (the official document number by which the document is identified by the originating activity. This number must be unique to this document).  	<b>10b. OTHER DOCUMENT NOS.</b> (Any other numbers which may be assigned this document either by the originator or by the sponsor).  <p style="text-align: center; font-size: large;">DREA/CR/93/482</p>	
<b>11. DOCUMENT AVAILABILITY</b> (any limitations on further dissemination of the document, other than those imposed by security classification)  <input checked="" type="checkbox"/> Unlimited distribution <input type="checkbox"/> Distribution limited to defence departments and defence contractors; further distribution only as approved <input type="checkbox"/> Distribution limited to defence departments and Canadian defence contractors; further distribution only as approved <input type="checkbox"/> Distribution limited to government departments and agencies; further distribution only as approved <input type="checkbox"/> Distribution limited to defence departments; further distribution only as approved <input type="checkbox"/> Other (please specify):		
<b>12. DOCUMENT ANNOUNCEMENT</b> (any limitation to the bibliographic announcement of this document. This will normally correspond to the Document Availability (11). However, where further distribution (beyond the audience specified in 11) is possible, a wider announcement audience may be selected).  <p style="text-align: center; font-size: large;">No limitation</p>		

**UNCLASSIFIED**  
SECURITY CLASSIFICATION OF FORM

DCD03 2/06/87-M

**UNCLASSIFIED**  
SECURITY CLASSIFICATION OF FORM

13. **ABSTRACT** (a brief and factual summary of the document. It may also appear elsewhere in the body of the document itself. It is highly desirable that the abstract of classified documents be unclassified. Each paragraph of the abstract shall begin with an indication of the security classification of the information in the paragraph (unless the document itself is unclassified) represented as (S), (C), (R), or (U). It is not necessary to include here abstracts in both official languages unless the text is bilingual).

The ferroelectric copolymer poly(vinylidene difluoride-trifluoroethylene) shows considerable promise as a transducer material for sonar transducers. This material has a low density, is flexible and has a hydrostatic figure of merit which can be an order of magnitude better than that of lead zirconate titanate which is currently the most commonly used transducer material. We have investigated a 0.500 mm thick copolymer with thin flexible aluminum coated nickel electrodes manufactured by AMP Sensors Ltd. of the USA. We have determined the elastic, dielectric, piezoelectric and hydrostatic properties of the copolymer with the flexible electrodes. The hydrostatic voltage coefficient and the hydrostatic figure of merit of this copolymer sample are at least five times better than those of lead zirconate titanate but they are not as good as values for the same copolymer with stiff electrodes which were investigated earlier. These properties have a small dependence on pressure and in this regard the present material is better than other polymers studied earlier.

14. **KEYWORDS, DESCRIPTORS or IDENTIFIERS** (technically meaningful terms or short phrases that characterize a document and could be helpful in cataloguing the document. They should be selected so that no security classification is required. Identifiers, such as equipment model designation, trade name, military project code name, geographic location may also be included. If possible keywords should be selected from a published thesaurus. e.g. Thesaurus of Engineering and Scientific Terms (TEST) and that thesaurus-identified. If it not possible to select indexing terms which are Unclassified, the classification of each should be indicated as with the title).

Piezoelectric polymers  
Hydrophone applications  
Hydrostatic properties  
Figure of merit

**UNCLASSIFIED**  
SECURITY CLASSIFICATION OF FORM

142296